| REVISIONS |  |  |  |
| :---: | :---: | :---: | :---: |
| REV | DESCRIPTION | DATE | APPROVED |
| A | REVISED GLAZING DETAILS | $04 / 14 / 17$ | R.L. |

1. THE PRODUCT SHOWN HEREIN IS DESIGNED AND MANUFACTURED TO COMPLY WITH REQUIREMENTS OF THE FLORIDA BUILDING CODE INCLUDING THE HVHZ.
2. WOOD FRAMING AND MASONRY OPENING TO BE DESIGNED AND ANCHORED TO PROPERLY TRANSFER ALL LOADS TO STRUCTURE. FRAMING AND MASONRY OPENING IS THE RESPONSIBILITY OF THE ARCHITECT OR ENGINEER OF RECORD.
3. SHIM AS REQUIRED AT EACH ANCHOR LOCATION WITH LOAD BEARING SHIM. SHIM WHERE SPACE OF 1/16" OR GREATER OCCURS. MAXIMUM ALLOWABLE SHIM STACK TO BE $1 / 2$ ".
4. SHIMS SHALL BE LOCATED, APPLIED AND MADE FROM MATERIALS AND THICKNESS CAPABLE OF SUSTAINING APPLICABLE LOADS
5. WIND LOAD DURATION FACTOR Cd=1.6 WAS USED FOR WOOD ANCHOR CALCULATIONS.
6. FRAME MATERIAL: EXTRUDED ALUMINUM 6063-T6
7. UNITS MUST BE GLAZED PER ASTM E1300-04/09, SEE SHEET 9 FOR GLASS DETAILS
8. APPROVED IMPACT PROTECTIVE SYSTEM IS NOT REQUIRED FOR THIS PRODUCT IN WIND BORNE DEBRIS REGIONS WHEN INSTALLED AT 3OFT OR HIGHER ABOVE GROUND LEVEL.
9. FOR ANCHORING INTO WOOD FRAMING OR $2 X$ BUCK USE $1 / 2$ " LAG SCREWS WITH SUFFICIENT LENGTH TO ACHIEVE A 2 " MINIMUM EMBEDMENT INTO SUBSTRATE. LOCATE ANCHORS AS SHOWN IN ELEVATIONS AND INSTALLATION DETAILS.
10. FOR ANCHORING INTO GROUT FILLED MASONRY OR CONCRETE USE $1 / 2$ " WEDGE BOLTS WITH SUFFICIENT LENGTH TO ACHIEVE A $31 / 2^{\prime \prime}$ MINIMUM EMBEDMENT INTO SUBSTRATE WITH 6" MINIMUM EDGE DISTANCE. LOCATE ANCHORS AS SHOWN IN ELEVATIONS AND INSTALLATION DETAILS.
11. FOR ANCHORING INTO METAL STRUCTURE USE $1 / 2-13$ SMS WITH LOCKWASHER AND NUT. LOCATE ANCHORS AS SHOWN IN ELEVATIONS AND INSTALLATION DETAILS
12. ALL FASTENERS TO BE CORROSION RESISTANT
13. INSTALLATION ANCHORS SHALL BE INSTALLED IN ACCORDANCE WITH ANCHOR MANUFACTURER'S INSTALLATION INSTRUCTIONS AND ANCHORS SHALL NOT BE USED IN SUBSTRATES WITH STRENGTHS LESS THAN THE MINIMUM STRENGTH SPECIFIED BELOW:
A. WOOD: MINIMUM SPECIFIC GRAVITY OF $G=0.42$
B. CONCRETE: MINIMUM COMPRESSIVE STRENGTH OF 2,000 PS
C. MASONRY: GROUT FILLED BLOCK PER ASTM C90 WITH Fm=2,000PSI MINIMUM
D. METAL STRUCTURE: STEEL $1 / 4$ " THICK MINIMUM $F Y=33 \mathrm{KSI} / F U=52 \mathrm{KSI}$

|  | TABLE OF CONTENTS | DIVISION OF C.R. LAURENCE CO., INC.2503 E. VERNON AVE., LOS ANGELES, CA 90058 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SHEET NO. | DESCRIPTION | STORM WALL XL HURRICANE RESISTANT CURTAIN WALL - DRY GLAZED - LMI HVHZ |  |  |  |  |
| 1 | NOTES |  |  |  |  |  |
| 2-4 | ELEVATIONS AND RATING CHARTS | DRAWN: R.L. | DWG No. |  |  | ( ReV |
| 5-8 | CROSS SECTIONS |  |  | 08-03022 |  |  |
| 9 | GLAZING DETAILS | SCALE NTS | DATE 12/07/16 | SHEET 1 OF 23 |  |  |
| 10-20 | INSTALLATION DETAILS | L. ROBERTO LOMAS P.E. <br> 1432 WOODFORD RD LEWISVILLE, NC 27023 434-688-0609 rllomas@Irlomaspe.com |  |  |  |  |
| 21-23 | COMPONENTS |  |  |  |  |  |  |

SIGNED: 04/17/2017 LAURENCE CO., INC. STORM WALL XL HURRICANE RESISTANT REV
A

21-23 COMPONENTS



| Chart \#1 <br> Design pressure for Mullion " $A$ ", " $B$ " and " $C$ " (psf) Design pressure for Jamb "B" and "C" (psf) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|c\|} \hline \text { Frame } \\ \text { Height } \\ \text { (in) } \end{array}$ | Design pressures are positive and negative Tributary Width (in) |  |  |  |  |  |  |  |  |
|  | 24.0 | 30.0 | 36.0 | 42.0 | 48.0 | 54.0 | 60.0 | 66.0 | 72.0 |
| 60.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 66.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 72.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 78.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 84.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 90.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 96.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 102.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 108.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 114.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 120.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 126.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 69.4 |
| 132.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 66.3 |
| 138.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 69.2 | 63.4 |
| 144.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 66.3 | 60.8 |
| 150.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 63.6 | 58.3 |

LARGE MISSILE IM PACT AND HVHZ

## Chart \#3

Chart \#3
Design pressure for Mullion " $A$ ", " $B$ " and " $G$ " (psf)

| Design pressure for Mullion " A ", " B " and " G " (psf) Design pressure for Jamb "C" and Corner (psf) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Frame } \\ \text { Height } \\ \text { (in) } \end{gathered}$ | Design pressures are positive and negative Tributary Width (in) |  |  |  |  |  |  |  |  |
|  | 24.0 | 30.0 | 36.0 | 42.0 | 48.0 | 54.0 | 60.0 | 66.0 | 72.0 |
| 60.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 66.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 72.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 78.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 84.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 90.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 96.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 102.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 108.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 114.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 120.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 126.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 69.4 |
| 132.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 66.3 |
| 138.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 69.2 | 63.4 |
| 144.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 66.3 | 60.8 |
| 150.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 63.6 | 58.3 |
| 156.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 69.1 | 62.2 | 56.6 | 51.9 |
| 162.0 | 70.0 | 70.0 | 70.0 | 70.0 | 69.5 | 61.7 | 55.6 | 50.5 | 46.3 |
| 168.0 | 70.0 | 70.0 | 70.0 | 70.0 | 62.3 | 55.4 | 49.8 | 45.3 | 41.5 |
| 174.0 | 70.0 | 70.0 | 70.0 | 64.1 | 56.1 | 49.8 | 44.8 | 40.8 | 37.4 |
| 175.0 | 70.0 | 70.0 | 70.0 | 63.0 | 55.1 | 49.0 | 44.1 | 40.1 | 36.7 |

LARGE MISSILE IM PACT AND HVHZ
FULL LENGTH WITHOUT SPLICE


LARGE MISSILE IM PACT AND HVHZ

## Chart\#4

Design pressure for Mullion " $A$ ", " $B$ " and " $G$ " with splice ( $p s f$ )

| Frame Height (in) | Design pressures are positive and negative Tributary Width (in) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 24.0 | 30.0 | 36.0 | 42.0 | 48.0 | 54.0 | 60.0 | 66.0 | 72.0 |
| 210.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 216.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 222.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 228.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 234.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 240.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 246.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 252.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 258.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 264.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 270.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 276.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 68.7 |
| 282.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 67.2 |
| 288.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 65.8 |
| 294.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 64.5 |
| 300.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 68.9 | 63.2 |
| 306.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 67.6 | 62.0 |
| 312.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 66.3 | 60.8 |
| 318.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 65.0 | 59.6 |
| 324.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 63.8 | 58.5 |
| 325.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 63.6 | 58.3 |

FULL LENGTH WITH SUPPORTT AT MIDDLE POINT AND SPLICE distance between splice and mid point must not exceed $25^{*}$

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US ALUMINUM
DIVISION OF C.R. LAURENCE CO., INC.

$$
2503 \text { E. VERNON AVE., LOS ANGELES, CA } 90058
$$

STORM WALL XL HURRICANE RESISTANT CURTAN WALL - DRY GLAZED - LMI HVHZ MULLION AND JAMB CHARTS

| $\begin{array}{\|l\|} \hline \text { DRAWN: } \\ \text { R.L. } \end{array}$ |  | DWG No. 08-03022 |  |  |  | $\begin{gathered} \text { REV } \\ A \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SCALE NTS | DATE | 12/07/16 | ${ }^{\text {SHEET }} 4$ | OF | 23 |  |




SIGNED: 04/17/2017




| REVISIONS |  |  |  |
| :---: | :---: | :---: | :---: |
| REV | DESCRIPTION | DATE | APPROVED |
| A | REVISED GLAZING DETAILS | $04 / 14 / 17$ | R.L. |












\section*{Chart \#}| 66.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 72.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
|  | 70.0 |  | 0.0 | 0.0 |  |  |  |  |  || 78.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 70.0 |  | 70.0 |  |  |  |  |  |  || 84.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: || 90.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 90.0 |  |  |  |  |  |  |  |  || 96.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1020 | 70.0 | 70.0 | 0.0 |  |  |  |  |  |  || $\mathbf{1 0 2 . 0}$ | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 108.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 || 108.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 114.0 | 700 | 70.0 | 70.0 | 70.0 | 70.0 | 70. | 70.0 | 70.0 | 70.0 |


| 114.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1 2 0 . 0}$ | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 || 126.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1 2 6 . 0}$ | 70.0 | 70.0 |  |  |  |  |  |  |  || 132.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- || 138.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: || 144.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 150.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 7.0 | 70.0 || $\mathbf{1 5 0 . 0}$ | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 156.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 || $\mathbf{1 5 6 . 0}$ | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1 6 2 . 0}$ | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 || 168.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- || 174.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1 7 5 . 0}$ | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |

Chart \#
Design pressure for anchoring into wood with (2) anchors per clip


 \begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline 60.0 \& 70.0 \& 700.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 <br>
\hline 60.0 \& 70.0 <br>
\hline $\mathbf{6 6 . 0}$ \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 <br>
\hline 70.0 <br>
\hline

 

\hline 66.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 <br>
\hline 72.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 <br>
\hline

 

\hline 78.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 <br>
\hline

 

\hline 84.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 <br>
\hline 90.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 68.9 <br>
\hline

 

\hline 90.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 68.9 <br>
\hline \& 10.0 \& \& <br>
\hline

 

\hline 96.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 64.6 <br>
\hline $\mathbf{1 0 . 0}$ \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& \& 6 <br>
\hline

 

\hline $\mathbf{1 0 2 . 0}$ \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 66.3 \& 60.8 <br>
\hline $\mathbf{1 0 8 . 0}$ \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 68.9 \& 62.6 \& 57.4 <br>
\hline

 

\hline $\mathbf{1 0 8 . 0}$ \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 68.9 \& 62.6 \& 57.4 <br>
\hline 114.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 653 \& 593 \& 54.4 <br>
\hline 12.0 \& 7.0 \& 7.0 \& 70.0 \& 7.0 \& 70.0 \& 6.9 \& 62.0 \& 56.4 \& 51.7 <br>
\hline

 

114.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 65.3 \& 59.3 \& 54.4 <br>
\hline $\mathbf{1 2 0 . 0}$ \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 68.9 \& 62.0 \& 56.4 \& 51.7 <br>
\hline 120.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 656 \& 59.0 \& 537 \& 492 <br>
\hline

 

\hline $\mathbf{1 2 6 . 0}$ \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 65.6 \& 59.0 \& 53.7 \& 49.2 <br>
\hline

 

\hline $\mathbf{1 3 2 . 0}$ \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 62.6 \& 56.4 \& 51.2 <br>
\hline $\mathbf{1 3 8 . 0}$ \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 67.4 \& 59.9 \& 53.9 \& 49.0 <br>
\hline

 

\hline 144.0 \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 64.6 \& 57.4 \& 51.7 \& 47.0 \& 43.1 <br>
\hline

 

$\mathbf{1 4 . 0}$ \& 70.0 \& 0.0 \& 10.0 \& 0.0 \& 64.6 \& 5.4 \& 51.7 \& 4.0 \& 43.1 <br>
\hline $\mathbf{1 5 0 . 0}$ \& 70.0 \& 70.0 \& 70.0 \& 70.0 \& 62.0 \& 55.1 \& 49.6 \& 45.1 \& 41.3 <br>
\hline $\mathbf{1 5 6 . 0}$ \& 70.0 \& 70.0 \& 70.0 \& 681 \& 59.6 \& 53.0 \& 477 \& 434 \& 39.7 <br>
\hline

 

\hline $\mathbf{1 5 6 . 0}$ \& 70.0 \& 70.0 \& 70.0 \& 68.1 \& 59.6 \& 53.0 \& 47.7 \& 43.4 \& 39.7 <br>
\hline $\mathbf{1 6 2 . 0}$ \& 70.0 \& 70.0 \& 70.0 \& 65.6 \& 57.4 \& 51.0 \& 45.9 \& 41.8 \& 38.3 <br>
\hline

 

162.0 \& 70.0 <br>
\hline 168.0 \& 70.0 \& 70.0 \& 70.0 \& 63.3 \& 55.4 \& 49.2 \& 44.3 \& 40.3 \& 38.3 <br>
\hline

 

\hline $\mathbf{1 7 4 . 0}$ \& 70.0 \& 70.0 \& 70.0 \& 61.1 \& 53.4 \& 47.5 \& 42.8 \& 38.9 \& 35.6 <br>
\hline $\mathbf{1 7 5 . 0}$ \& 70.0 \& 70.0 \& 70.0 \& 60.7 \& 53.1 \& 47.2 \& 42.5 \& 38.6 \& 35.4 <br>
\hline
\end{tabular}

## Chart \#8

Design pressure for anchoring
into wood with (4) anchors per clip or
into metal or concrete with (2) or (4) anchors per clip

| $\begin{array}{\|c\|} \hline \text { Frame } \\ \text { Height (in) } \end{array}$ | Tributary width (in) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 24.0 | 30.0 | 36.0 | 42.0 | 48.0 | 54.0 | 60.0 | 66.0 | 72.0 |
| 60.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 66.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 72.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 78.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 84.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 90.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 96.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 102.0 | 0.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 108.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 114.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 120.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 126.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 132.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 138.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 144.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 150.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 156.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 162.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 168.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 174.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 75.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |

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