



**Project No.:** 27206.10-107-16  
**Project Name:** Contours S.E. ISW/OSW Opaque  
w/Dunbarton RedI-Flex 90min Frame  
**Date:** 9/28/2023  
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## **PRODUCT APPROVAL SUPPORTING CALCULATIONS**

**Series/Model Contours S.E. ISW/OSW Opaque w/Dunbarton RedI-Flex 90min Frame**

**REPORT No.:** 27206.10-107-16

**RENDERED TO:** Jeld-Wen Windows & Doors  
3737 Lakeport Blvd  
Klamath Falls, Oregon

**PREPARED BY:** Michael D. Stremmel, P.E.  
Molimo, LLC  
1410 Eden Road  
York, Pennsylvania 17402

**DATE:** 9/28/2023

This item has been digitally signed and sealed by Michael D. Stremmel, PE on the date adjacent to the seal.

Printed copies of this document are not considered signed and sealed and the signature must be verified on electronic copies.

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Michael D. Stremmel, P.E.  
Senior Project Engineer  
FL PE 65868  
FL REG 37122

*It is a violation to alter this document in any way unless acting under the direction of a licensed professional engineer.*



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**SCOPE:**

Molimo, LLC was contracted by Jeld-Wen Windows & Doors to evaluate alternate installation methods for their Contours S.E. ISW/OSW Opaque w/Dunbarton RedI-Flex 90min Frame. The evaluation is based on physical testing and product certifications.

Reference standards utilized in this project include:

*Florida Building Code.* International Code Council.

*ANSI/AWC National Design Specification (NDS) for Wood Construction.* American Wood Council.

*AISI S100 North American Specification for the Design of Cold-Formed Steel Structural Members.* American Iron and Steel Institute.

ICC-ES Report ESR-1976 ITW Buildex TEKS Self-Drilling Fasteners. ICC Evaluation Service.

NOA 21-0201.06 *Tapcon Concrete and Masonry Anchors with Advanced Threadform Technology.* Miami-Dade County Product Control Section.

The anchorage analysis presented herein does not address the water resistance, water penetration, or air infiltration performance of the installation method or the installed product. In addition, the analyses rely on the assumption that the building substrate is capable of withstanding the incurred loads.



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### Certification of Independence

In accordance with Rule 61G20-3 Florida Administrative Code, Molimo, LLC hereby certifies the following:

- Molimo, LLC does not have, nor does it intend to acquire or will it acquire, a financial interest in any company manufacturing or distributing products tested or labeled by the agency.
- Molimo LLC is not owned, operated or controlled by any company manufacturing or distributing products it tests or labels.
- Michael D. Stremmel, P.E. does not have nor will acquire, a financial interest in any company manufacturing or distributing products for which the reports are being issued.
- Michael D. Stremmel, P.E. does not have, nor will acquire, a financial interest in any other entity involved in the approval process of the product.

## ANALYSES:

### Summary of Test Results

Table 1 summarizes the various Contours S.E. ISW/OSW Opaque w/Dunbarton Redi-Flex 90min Frame products and their corresponding performance levels which have been established by testing or product certification.

**Table 1:** Summary of Test Results

Series/Model	Test Report Number	Size (W x H)	Performance
Contours Premium Steel Door w/steel Edge Opaque In-Swing Door (ADA Threshold)	National Certified Testing Laboratories Report No. NCTL-210-3844-1 (Rev. 0, 10/29/12) and NCTL-210-3844-1A (Rev. 0, 10/29/12)	38-15/16" x 86-5/8"	+47 / -47 psf (Wind Zone 4)
Contours Premium Steel Door w/steel Edge Opaque Out-Swing Door (Standard Threshold)		38-15/16" x 85-3/8"	+66 / -66 psf (Wind Zone 4)

Testing documented in Table 1 was conducted by National Certified Testing Laboratories of Orlando, Florida (Florida Department of Business & Professional Regulation Test Lab No. TST1589 – laboratory was approved at the time of testing). The testing documented above is certified by NAMI under certification number NI011401.01-R6 (Expires 10/31/2026) and NI011401.02-R6 (Expires 10/31/2026)

### As-Tested Installation Analysis

For air/water/structural testing, the test specimen was secured to a Southern-Yellow-Pine wood test buck with #10 wood screws (1-1/2" min. embedment) at the head and jambs and a continuous bed of silicone at the sill. The as tested installation method is evaluated on [Pages 5 and 6](#). These capacities will be used to prove acceptable anchors and substrates for the product.

### Alternate Anchorages

Calculations on [Pages 7 through 13](#) determine the design capacity of alternate installation anchorages for the product.

### Anchorages Requirements

As-tested spacing must be maintained. It must be determined that the anchorages are not overloaded for the approved product size and design pressures. Calculations presented on Page 14 show the alternate anchorages are acceptable for the established product performance.

Anchorage requirements established by this report are accurately presented in Drawing D015882.

**As-Tested Installation – Through Frame to Wood**

Anchor: #6 Wood screws (1-1/2" Min Embedment) Head, Jamb

Details: 16 ga (0.060") thick steel door frame  
No shim space was utilized

Substrate: Southern-Yellow-Pine wood test buck (G = 0.55)

**Wood Screw Capacity (#6 Wood Screw Shear)**

Z' = 126 lb

(See Following Page)

**Design Capacity of the Connection = 126 lb**

## Lateral Design Strength of Wood Connections

### Data

#### Fastener

Fastener	=	#6 Wood Screw
Shank Dia	=	0.138 in.
Root Dia.	=	0.113 in.
$F_{yb}$	=	100,000 psi
Fastener length	=	2.250 in.

**Project:** Countours S.E. Isw Opaque  
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**Comments:** As-Tested  
 1-1/2" min embedment

#### Main Member

Material	=	SYP
G	=	0.55
$\theta$	=	90
$F_e$	=	5,550 psi
Thickness	=	1.500 in.

#### Side Member

Material	=	ASTM A 653, Grade 33 Steel
G	=	N/A
$\theta$	=	90
$F_{es}$	=	61,850 psi
Thickness	=	0.060 in.

### Calculations

#### Lateral Bearing Factors

D	=	0.113 in.
$\ell_m$	=	1.500 in.
$K_\theta$	=	1.25
$K_D$	=	2.20
$R_e$	=	0.090
$R_t$	=	25.00

$k_1$	=	0.9060
$k_2$	=	0.5033
$k_3$	=	9.65
$R_d$	=	2.20 (Mode I <sub>m</sub> , I <sub>s</sub> )
$R_d$	=	2.20 (Mode II)
$R_d$	=	2.20 (Mode III <sub>m</sub> , III <sub>s</sub> , IV)

#### Lateral Design Values, Z

Mode I <sub>m</sub>	=	428 lbf
Mode I <sub>s</sub>	=	191 lbf
Mode II	=	173 lbf
Mode III <sub>m</sub>	=	182 lbf
Mode III <sub>s</sub>	=	79 lbf
Mode IV	=	107 lbf

<== Minimum Value

#### Adjustment Factors

$C_D$	=	1.6
Wet Service Factor		
Fabrication/In-Service	Dry/Dry	
$C_M$	=	1.0
In service temperature	$T \leq 100^\circ\text{F}$	
$C_t$	=	1.0
$C_g$	=	1.0

$C_\Delta$	=	1.0
Is fastener installed in end grain?	No	
$C_{eg}$	=	1.00
Is fastener part of a diaphragm?	No	
$C_{di}$	=	1.0
Is fastener toe-nailed?	No	
$C_{tn}$	=	1.00

#### Adjusted Design Value, Z'

Z'	=	126 lbf
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**Alternate Installation – Through-Frame to Concrete**

Anchor: 1/4" Tapcon Anchor  
- 1-1/4" min embedment  
- 2-1/2" min edge distance  
- 3" min anchor spacing  
- 1/4" max shim space

Details: 16 ga (0.060") thick steel door frame

Substrate: 3,000 psi Concrete

Anchor Capacity (Shear of 1/4" Tapcon)

$$P_{ss} / \Omega = \underline{223 \text{ lb}} \quad (\text{NOA-No. 21-0201.06})$$

Bearing Capacity (of Steel frame)

$$P_b = 0.85 F_e D t / K_D = 0.85 (45,000 \text{ psi})(0.250")(0.060") / (3.0) = \underline{191 \text{ lb}}$$

Bending Capacity (of 1/4" Tapcon)

$$L = 1/4" \text{ (maximum shim space)}$$

$$S = \pi d^3 / 32 = \pi (0.190")^3 / 32 = 0.000673 \text{ in}^3$$

$$F_b = (1.3)(0.6 F_y) = (1.3)(0.6)(137,000 \text{ psi}) = 106,860 \text{ psi} \quad (1.3 \text{ for weak axis bending})$$

$$F_b = M / S = (V) (L/2) / S \quad (L/2 \text{ for guided bending})$$

$$V = 2 S F_b / L = (2)(0.000673 \text{ in}^3)(106,860 \text{ psi}) / 1/4"$$

$$V = \underline{575 \text{ lb}}$$

**Design Capacity of the Connection = 191 lb**

**Alternate Installation – Through-Frame to CMU Block**

Anchor: 3/16" Tapcon Anchor  
- 1-1/4" min embedment  
- 2-1/2" min edge distance  
- 3" min anchor spacing  
- 1/4" max shim space

Details: 16 ga (0.060") thick steel door frame

Substrate: CMU Block

Anchor Capacity (Shear of 1/4" Tapcon)

$$P_{ss} / \Omega = \underline{161 \text{ lb}} \quad (\text{NOA-No. 21-0201.06})$$

Bearing Capacity (of Steel frame)

$$P_b = 0.85 F_e D t / K_D = 0.85 (45,000 \text{ psi})(0.250")(0.060") / (3.0) = \underline{191 \text{ lb}}$$

Bending Capacity (of 1/4" Tapcon)

$$L = 1/4" \text{ (maximum shim space)}$$

$$S = \pi d^3 / 32 = \pi (0.190")^3 / 32 = 0.000673 \text{ in}^3$$

$$F_b = (1.3)(0.6 F_y) = (1.3)(0.6)(137,000 \text{ psi}) = 106,860 \text{ psi} \quad (1.3 \text{ for weak axis bending})$$

$$F_b = M / S = (V) (L/2) / S \quad (L/2 \text{ for guided bending})$$

$$V = 2 S F_b / L = (2)(0.000673 \text{ in}^3)(106,860 \text{ psi}) / 1/4"$$

$$V = \underline{575 \text{ lb}}$$

**Design Capacity of the Connection = 161 lb**



### Anchorage Requirements

Series/Model: Opaque Steel Edge Door (In-Swing & Out-Swing)  
Test Unit Size: 38 47/50" x 86 63/100"  
38 47/50" x 85 19/50"  
Design Pressure: +47.0 / -47.0 psf  
+66.0 / -66.0 psf

### Through-Frame Installation Method

Through frame installation method is validated by the test

Through Frame Anchor Capacity = 126 lb / anchor

### Alternate Installation Methods

Through-Frame to Concrete = 191 lb / anchor

Through-Frame to CMU Block = 161 lb / anchor

Minimum Alternate Installation Capacity = 161 lb / anchor

126 lb < 161 lb

### Alternate Anchorages OK at tested spacing



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### Revision Log

<b>Rev. #</b>	<b>Date</b>	<b>Page(s)</b>	<b>Revision(s)</b>
0	9/28/2023	All	Original Report Issue