



Project No.: 27561.11-107-16
Project Name: Contours Steel Wood Edge
Inswing Glazed OXXO
Date: 11/17/2023
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PRODUCT APPROVAL SUPPORTING CALCULATIONS

Series/Model: Contours Steel Wood Edge Inswing Glazed OXXO

REPORT No.: 27561.11-107-16

RENDERED TO: Jeld-Wen Windows & Doors
3737 Lakeport Blvd
Klamath Falls, Oregon

PREPARED BY: Michael D. Stremmel, P.E.
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DATE: 11/17/2023

This item has been digitally signed and sealed by Michael D. Stremmel, PE on the date adjacent to the seal.

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Michael D. Stremmel, P.E.
Senior Project Engineer
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FL REG 37122

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SCOPE:

Molimo, LLC was contracted by Jeld-Wen Windows & Doors to evaluate alternate installation methods for their Contours Steel Wood Edge Inswing Glazed OXXO. The evaluation is based on physical testing and product certifications.

Reference standards utilized in this project include:

Florida Building Code. International Code Council.

ANSI/AWC National Design Specification (NDS) for Wood Construction. American Wood Council.

AISI S100 North American Specification for the Design of Cold-Formed Steel Structural Members. American Iron and Steel Institute.

ICC-ES Report ESR-1976 ITW Buildex TEKS Self-Drilling Fasteners. ICC Evaluation Service.

NOA 21-0201.06 *Tapcon Concrete and Masonry Anchors with Advanced Threadform Technology.* Miami-Dade County Product Control Section.

The anchorage analysis presented herein does not address the water resistance, water penetration, or air infiltration performance of the installation method or the installed product. In addition, the analyses rely on the assumption that the building substrate is capable of withstanding the incurred loads.



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Certification of Independence

In accordance with Rule 61G20-3 Florida Administrative Code, Molimo, LLC hereby certifies the following:

- Molimo, LLC does not have, nor does it intend to acquire or will it acquire, a financial interest in any company manufacturing or distributing products tested or labeled by the agency.
- Molimo LLC is not owned, operated or controlled by any company manufacturing or distributing products it tests or labels.
- Michael D. Stremmel, P.E. does not have nor will acquire, a financial interest in any company manufacturing or distributing products for which the reports are being issued.
- Michael D. Stremmel, P.E. does not have, nor will acquire, a financial interest in any other entity involved in the approval process of the product.

ANALYSES:

Summary of Test Results

Table 1 summarizes the various Contours Steel Wood Edge Inswing Glazed OXXO products and their corresponding performance levels which have been established by testing or product certification.

Table 1: Summary of Test Results

| Series/Model | Test Report Number | Size (W x H) | Performance |
|--|---|--------------------------|-------------------------------|
| Jeld-Wen, INC. Steel 24 GA W.E. Double Door with Fixed Sidelites | National Certified Testing Laboratories Report No. NCTL-210-3804-3 (3/01/2012) | 149" x 98" (In-Swing) | +35 / -35 psf (non-impact) |

Testing documented in Table 1 was conducted by National Certified Testing Laboratories of Orlando, Florida (Florida Department of Business & Professional Regulation Test Lab No. TST1589 – laboratory was approved at the time of testing). The testing documented above is certified by NAMI under certification number NI011064-R7 (Expires 4/30/2026).

As-Tested Installation Analysis

For air/water/structural testing, the test specimen was secured to a Southern-Yellow-Pine wood test buck with #10 wood screws (1-1/2" min. embedment) at the head, sill, and jambs. The as tested installation method is evaluated on Pages 5 and 6. These capacities will be used to prove acceptable anchors and substrates for the product.

Alternate Anchorages

Calculations on Pages 7 through 13 determine the design capacity of alternate installation anchorages for the product.

Anchorages Requirements

As-tested spacing must be maintained. It must be determined that the anchorages are not overloaded for the approved product size and design pressures. Calculations presented on Page 14 show the alternate anchorages are acceptable for the established product performance.

Anchorage requirements established by this report are accurately presented in Drawing D015859.



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As-Tested Installation – Through Frame to Wood

Anchor: #10 x 3" Wood Screw
(1-1/2" min embedment})

Details: 0.719" thick wood frame (G = 0.42)
No shim space was utilized.

Substrate: Southern-Yellow-Pine wood test buck (G = 0.55)

Wood Screw Capacity (Shear)

Z' = 143 lb

(See Following Page)

Design Capacity of the Connection = 143 lb

Lateral Design Strength of Wood Connections

Data

Fastener

| | | |
|-----------------|---|----------------|
| Fastener | = | #10 Wood Screw |
| Shank Dia | = | 0.190 in. |
| Root Dia. | = | 0.152 in. |
| F_{yb} | = | 80,000 psi |
| Fastener length | = | 2.250 in. |

| | |
|------------------|---|
| Project: | Contours Steel Wood Edge Inswing Glazed OXXO |
| Comments: | As-tested Installation 1-1/2" min embedment |

Main Member

| | | |
|-----------|---|-----------|
| Material | = | SYP |
| G | = | 0.55 |
| θ | = | 90 |
| F_e | = | 5,550 psi |
| Thickness | = | 1.500 in. |

Side Member

| | | |
|-----------|---|-----------|
| Material | = | SPF |
| G | = | 0.42 |
| θ | = | 90 |
| F_{es} | = | 3,350 psi |
| Thickness | = | 0.719 in. |

Calculations

Lateral Bearing Factors

| | | |
|------------|---|-----------|
| D | = | 0.152 in. |
| ℓ_m | = | 1.326 in. |
| K_θ | = | 1.25 |
| K_D | = | 2.20 |
| R_e | = | 1.657 |
| R_t | = | 1.84 |

| | | |
|-------|---|--|
| k_1 | = | 0.9248 |
| k_2 | = | 1.4204 |
| k_3 | = | 1.19 |
| R_d | = | 2.20 (Mode I _m , I _s) |
| R_d | = | 2.20 (Mode II) |
| R_d | = | 2.20 (Mode III _m , III _s , IV) |

Lateral Design Values, Z

| | | |
|-----------------------|---|---------|
| Mode I _m | = | 508 lbf |
| Mode I _s | = | 166 lbf |
| Mode II | = | 154 lbf |
| Mode III _m | = | 167 lbf |
| Mode III _s | = | 89 lbf |
| Mode IV | = | 111 lbf |

<== Minimum Value

Adjustment Factors

| | | |
|------------------------|---|----------------------------|
| C_D | = | 1.6 |
| Wet Service Factor | | |
| Fabrication/In-Service | = | Dry/Dry |
| C_M | = | 1.0 |
| In service temperature | = | $T \leq 100^\circ\text{F}$ |
| C_t | = | 1.0 |
| C_g | = | 1.0 |

| | | |
|-------------------------------------|---|------|
| C_Δ | = | 1.0 |
| Is fastener installed in end grain? | = | No |
| C_{eg} | = | 1.00 |
| Is fastener part of a diaphragm? | = | No |
| C_{di} | = | 1.0 |
| Is fastener toe-nailed? | = | No |
| C_{tn} | = | 1.00 |

Adjusted Design Value, Z

| | | |
|----|---|---------|
| Z' | = | 143 lbf |
|----|---|---------|

Alternate Installation – Strap Anchor to Wood

Anchor: #10 x 2" Flat head screw securing the strap to the substrate
1/4" max shim space

Details: 20 gauge (0.033" thick) 33 KSI steel strap anchor w/ two #10 screws securing the strap to the frame
1-1/2" thick wood frame

Substrate: Spruce-Pine-Fir 2x Wood Substrate (G = 0.42 min.)

Wood Screw Capacity (Shear)

$$Z' = \underline{155 \text{ lb}}$$

(See Following Page)

Bending of #10 x 2" flat head screw

$$L = 1/4" \text{ (maximum shim space)}$$

$$S = \pi d^3 / 32 = \pi (0.145")^3 / 32 = 0.000299 \text{ in}^3$$

$$F_b = (1.3)(0.6 F_y) = (1.3)(0.6)(90,000 \text{ psi}) = 70,200 \text{ psi} \quad (1.3 \text{ for weak axis bending})$$

$$F_b = M / S = (V) (L/2) / S \quad (L/2 \text{ for guided bending})$$

$$V = 2 S F_b / L = (2)(0.000299 \text{ in}^3)(70,200 \text{ psi}) / 1/4"$$

$$V = \underline{168 \text{ lb}}$$

Bearing Capacity (of #10 screw on frame)

$$P_b = F_e D t / K_D = (3,350 \text{ psi})(0.164")(0.719") / (10(0.164) + 0.5) = \underline{184 \text{ lb}}$$

Bearing Capacity (of strap anchor)

$$P_b = 2.7 D t F_{tu} = 2.7(0.164")(0.033")(45,000 \text{ psi}) = 657 \text{ lb}$$

$$P_{\text{allow}} = 657 \text{ lb} / 3.0 = \underline{219 \text{ lb}}$$

Design Capacity of the Connection = 155 lb

Lateral Design Strength of Wood Connections

Data

Fastener

| | | |
|-----------------|---|----------------|
| Fastener | = | #10 Wood Screw |
| Shank Dia | = | 0.190 in. |
| Root Dia. | = | 0.152 in. |
| F_{yb} | = | 80,000 psi |
| Fastener length | = | 1.500 in. |

| | |
|------------------|--|
| Project: | Contours Steel Wood Edge Inswing Glazed OXXO |
| Comments: | Steel Strap Installation 1-1/2" min embedment |

Main Member

| | | |
|-----------|---|-----------|
| Material | = | SPF |
| G | = | 0.42 |
| θ | = | 90 |
| F_e | = | 3,350 psi |
| Thickness | = | 1.500 in. |

Side Member

| | | |
|-----------|---|----------------------------|
| Material | = | ASTM A 653, Grade 33 Steel |
| G | = | N/A |
| θ | = | 90 |
| F_{es} | = | 61,850 psi |
| Thickness | = | 0.033 in. |

Calculations

Lateral Bearing Factors

| | | |
|------------|---|-----------|
| D | = | 0.152 in. |
| ℓ_m | = | 1.277 in. |
| K_θ | = | 1.25 |
| K_D | = | 2.20 |
| R_e | = | 0.054 |
| R_t | = | 38.70 |

| | | |
|-------|---|--|
| k_1 | = | 0.8550 |
| k_2 | = | 0.5357 |
| k_3 | = | 26.07 |
| R_d | = | 2.20 (Mode I _m , I _s) |
| R_d | = | 2.20 (Mode II) |
| R_d | = | 2.20 (Mode III _m , III _s , IV) |

Lateral Design Values, Z

| | | |
|-----------------------|---|---------|
| Mode I _m | = | 296 lbf |
| Mode I _s | = | 141 lbf |
| Mode II | = | 121 lbf |
| Mode III _m | = | 143 lbf |
| Mode III _s | = | 97 lbf |
| Mode IV | = | 137 lbf |

<== Minimum Value

Adjustment Factors

| | | |
|------------------------|---|----------------------------|
| C_D | = | 1.6 |
| Wet Service Factor | | |
| Fabrication/In-Service | = | Dry/Dry |
| C_M | = | 1.0 |
| In service temperature | = | $T \leq 100^\circ\text{F}$ |
| C_t | = | 1.0 |
| C_g | = | 1.0 |

| | | |
|-------------------------------------|---|------|
| C_Δ | = | 1.0 |
| Is fastener installed in end grain? | = | No |
| C_{eg} | = | 1.00 |
| Is fastener part of a diaphragm? | = | No |
| C_{di} | = | 1.0 |
| Is fastener toe-nailed? | = | No |
| C_{tn} | = | 1.00 |

Adjusted Design Value, Z

| | | |
|----|---|---------|
| Z' | = | 155 lbf |
|----|---|---------|

Alternate Installation – Through-Frame to Concrete

Anchor: 3/16" Tapcon Anchor
- 1-1/4" min embedment
- 2-1/2" min edge distance
- 4" min anchor spacing
- 1/4" max shim space

Details: Through the Wood Frame
- 1" thick

Substrate: 3,000 psi Concrete

Anchor Capacity (Shear of 3/16" Tapcon)

$$P_{ss} / \Omega = \underline{181 \text{ lb}} \quad (\text{NOA-No. 16-1222.06})$$

Bearing Capacity (of Wood frame)

$$P_b = F_e D t / K_D = (3,350 \text{ psi}) (0.170") (1.00") / (10(0.170) + 0.5) = \underline{259 \text{ lb}}$$

Bending Capacity (of 3/16" Tapcon)

$$L = 1/4" \text{ (maximum shim space)}$$

$$S = \pi d^3 / 32 = \pi (0.170")^3 / 32 = 0.000482 \text{ in}^3$$

$$F_b = (1.3) (0.6 F_y) = (1.3) (0.6) (137,000 \text{ psi}) = 106,860 \text{ psi} \quad (1.3 \text{ for weak axis bending})$$

$$F_b = M / S = (V) (L/2) / S \quad (L/2 \text{ for guided bending})$$

$$V = 2 S F_b / L = (2) (0.000482 \text{ in}^3) (106,860 \text{ psi}) / 1/4"$$

$$V = \underline{412 \text{ lb}}$$

Design Capacity of the Connection = 181 lb

Qualifies 1/4" Tapcon if longer length anchor is required to achieve minimum embedment

Alternate Installation – Through-Frame to CMU Block

Anchor: 3/16" Tapcon Anchor
- 1-1/4" min embedment
- 2-1/2" min edge distance
- 4" min anchor spacing
- 1/4" max shim space

Details: Through the Wood Frame
- 1" thick

Substrate: CMU Block

Anchor Capacity (Shear of 3/16" Tapcon)

$$P_{ss} / \Omega = \underline{135 \text{ lb}} \quad (\text{NOA-No. 16-1222.06})$$

Bearing Capacity (of Wood frame)

$$P_b = F_e D t / K_D = (3,350 \text{ psi})(0.170")(1.00") / (10(0.170) + 0.5) = \underline{259 \text{ lb}}$$

Bending Capacity (of 3/16" Tapcon)

$$L = 1/4" \text{ (maximum shim space)}$$

$$S = \pi d^3 / 32 = \pi (0.170")^3 / 32 = 0.000482 \text{ in}^3$$

$$F_b = (1.3)(0.6 F_y) = (1.3)(0.6)(137,000 \text{ psi}) = 106,860 \text{ psi} \quad (1.3 \text{ for weak axis bending})$$

$$F_b = M / S = (V) (L/2) / S \quad (L/2 \text{ for guided bending})$$

$$V = 2 S F_b / L = (2)(0.000482 \text{ in}^3)(106,860 \text{ psi}) / 1/4"$$

$$V = \underline{412 \text{ lb}}$$

Design Capacity of the Connection = 135 lb

Qualifies 1/4" Tapcon if longer length anchor is required to achieve minimum embedment

Alternate Installation – Strap Anchor to Concrete

Anchor: 3/16" Tapcon Anchor
 - 1-1/4" min embedment
 - 2-1/2" min edge distance
 - 4" min anchor spacing
 - 1/4" max shim space

Details: 20 gauge (0.033" thick) 33 KSI steel strap anchor w/ two #8 screws securing the strap to the frame
 1.00" thick wood frame

Substrate: 3,000 psi Concrete

Anchor Capacity (Shear of 3/16" Tapcon)

$$P_{ss} / \Omega = \underline{181 \text{ lb}} \quad (\text{NOA-No. 16-1222.06})$$

Bearing Capacity (of 3/16" Tapcon on strap anchor)

$$P_b = 2.7 D t F_{tu} = 2.7(0.170")(0.033")(45,000 \text{ psi}) = 681 \text{ lb}$$

$$P_{\text{allow}} = 681 \text{ lb} / 3.0 = \underline{227 \text{ lb}}$$

Bearing Capacity (of #10 screw on frame)

$$P_b = F_e D t / K_D = (3,350 \text{ psi})(0.190")(1.00") / (10(0.164) + 0.5) = \underline{257 \text{ lb}}$$

Bearing Capacity (of #8 screw on strap anchor)

$$P_b = 2.7 D t F_{tu} = 2.7(0.164")(0.033")(45,000 \text{ psi}) = 657 \text{ lb}$$

$$P_{\text{allow}} = 657 \text{ lb} / 3.0 = \underline{219 \text{ lb}}$$

Bending Capacity (of 3/16" Tapcon)

$$L = 1/4" \text{ (maximum shim space)}$$

$$S = \pi d^3 / 32 = \pi (0.170")^3 / 32 = 0.000482 \text{ in}^3$$

$$F_b = (1.3)(0.6 F_y) = (1.3)(0.6)(137,000 \text{ psi}) = 106,860 \text{ psi} \quad (1.3 \text{ for weak axis bending})$$

$$F_b = M / S = (V) (L/2) / S \quad (L/2 \text{ for guided bending})$$

$$V = 2 S F_b / L = (2)(0.000482 \text{ in}^3)(106,860 \text{ psi}) / 1/4"$$

$$V = \underline{412 \text{ lb}}$$

Design Capacity of the Connection = 181 lb (one concrete anchor per strap)

Qualifies 1/4" Tapcon if longer length anchor is required to achieve minimum embedment

Alternate Installation – Strap Anchor to CMU Block

Anchor: 1/4" Tapcon Anchor
- 1-1/4" min embedment
- 2-1/2" min edge distance
- 4" min anchor spacing
- 1/4" max shim space

Details: 20 gauge (0.033" thick) 33 KSI steel strap anchor w/ two #10 screws securing the strap to the frame
1.00" thick wood frame

Substrate: CMU Block

Anchor Capacity (Shear of 1/4" Tapcon)

$$P_{ss} / \Omega = \underline{161 \text{ lb}} \quad (\text{NOA-No. 16-1222.06})$$

Bearing Capacity (of 1/4" Tapcon on strap anchor)

$$P_b = 2.7 D t F_{tu} = 2.7(0.190")(0.033")(45,000 \text{ psi}) = 762 \text{ lb}$$

$$P_{\text{allow}} = 762 \text{ lb} / 3.0 = \underline{254 \text{ lb}}$$

Bearing Capacity (of #8 screw on frame)

$$P_b = F_e D t / K_D = (3,350 \text{ psi})(0.164")(1.00") / (10(0.164) + 0.5) = \underline{257 \text{ lb}}$$

Bearing Capacity (of #8 screw on strap anchor)

$$P_b = 2.7 D t F_{tu} = 2.7(0.164")(0.033")(45,000 \text{ psi}) = 657 \text{ lb}$$

$$P_{\text{allow}} = 657 \text{ lb} / 3.0 = \underline{219 \text{ lb}}$$

Bending Capacity (of 1/4" Tapcon)

$$L = 1/4" \text{ (maximum shim space)}$$

$$S = \pi d^3 / 32 = \pi (0.190")^3 / 32 = 0.000673 \text{ in}^3$$

$$F_b = (1.3)(0.6 F_y) = (1.3)(0.6)(137,000 \text{ psi}) = 106,860 \text{ psi} \quad (1.3 \text{ for weak axis bending})$$

$$F_b = M / S = (V) (L/2) / S \quad (L/2 \text{ for guided bending})$$

$$V = 2 S F_b / L = (2)(0.000673 \text{ in}^3)(106,860 \text{ psi}) / 1/4"$$

$$V = \underline{575 \text{ lb}}$$

Design Capacity of the Connection = 161 lb (one concrete anchor per strap)

Qualifies 1/4" Tapcon if longer length anchor is required to achieve minimum embedment

Alternate Installation – Strap Anchor to Wood (Cap Installation)

Anchor: Two #8 x 1-1/2" Flat head screw securing the strap to the substrate

Details: 20 gauge (0.033" thick) 33 KSI steel strap anchor w/ two #8 screws securing the strap to the frame
1.00" thick wood frame
1/4" max shim space

Substrate: Spruce-Pine-Fir 2x Wood Substrate (G = 0.42 min.)

Wood Screw Capacity (Withdrawal)

$$W' = 1.6(82 \text{ lb/in})(1.5 \text{ in}) = \underline{197 \text{ lb}}$$

Pull-over Capacity (of #8 screw on strap)

$$P_{\text{nov}} = 1.5 t d F_{\text{tu}} = 1.5 (0.033")(0.332")(45,000 \text{ psi}) = 739 \text{ lb}$$

$$P_{\text{allow}} = 739 \text{ lb} / 3.0 = \underline{246 \text{ lb}}$$

Bearing Capacity (of #8 screw on frame)

$$P_b = F_e D t / K_D = (3,350 \text{ psi})(0.164")(1.00") / (10(0.164) + 0.5) = \underline{257 \text{ lb}}$$

Bearing Capacity (of #8 screw on strap anchor)

$$P_b = 2.7 D t F_{\text{tu}} = 2.7(0.164")(0.033")(45,000 \text{ psi}) = 657 \text{ lb}$$

$$P_{\text{allow}} = 657 \text{ lb} / 3.0 = \underline{219 \text{ lb}}$$

Design Capacity of the Connection = 197 lb (one screw)

Design Capacity of the Connection = 394 lb (two screws)

Anchorage Requirements

Series/Model: Contours Steel Wood Edge Inswing Glazed OXXO
Test Unit Size: 148-7/8" x 98"
Design Pressure: +35.0 / -35.0 psf

Through-Frame Installation Method

Through frame installation method is validated by the test

Through Frame Anchor Capacity = 143 lb / anchor

Alternate Installation Methods

Strap Anchor to Wood = 155 lb / anchor

Through-Frame to Concrete = 181 lb / anchor

Through-Frame to CMU Block = 135 lb / anchor

Strap Anchor to Concrete = 181 lb / anchor

Strap Anchor to CMU Block = 161 lb / anchor

Strap Anchor to Wood (Cap Installation) = 197 lb / anchor

Minimum Alternate Installation Capacity = 135 lb / anchor

135 lb < 143 lb

- Less than 6% difference, alternate anchorage is deemed equivalent (< 10%)
- Total Unit Load = (149")(98")/144 x 35 psf = 3,550 lb
- # of Anchors Utilized: Head/Sill = 14 anchors; Jambs = 6 anchors each
- Total Anchorage Capacity = (135 lb/anchor)(40 anchors) = 5,400 lb
- 5,400 lb > 3,550 lb

Alternate Anchorages OK at tested spacing



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Revision Log

| Rev. # | Date | Page(s) | Revision(s) |
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| 0 | 11/17/2023 | All | Original Report Issue |