



**Project No.:** 27226.01-107-16  
**Project Name:** F-4500 Fiberglass Folding  
Doors (Impact)  
**Date:** 9/29/2023  
Page 1 of 15

## PRODUCT APPROVAL SUPPORTING CALCULATIONS

Series/Model F-4500 Fiberglass Folding Doors (Impact)

REPORT NO.: 27226.01-107-16

RENDERED TO: Jeld-Wen Windows & Doors  
3737 Lakeport Blvd  
Klamath Falls, Oregon

PREPARED BY: Michael D. Stremmel, P.E.  
Molimo, LLC  
1410 Eden Road  
York, Pennsylvania 17402

DATE: 9/29/2023

This item has been digitally signed and sealed by Michael D. Stremmel, PE on the date adjacent to the seal.

Printed copies of this document are not considered signed and sealed and the signature must be verified on electronic copies.

---

Michael D. Stremmel, P.E.  
Senior Project Engineer  
FL PE 65868  
FL REG 37122

*It is a violation to alter this document in any way unless acting under the direction of a licensed professional engineer.*



**Project No.:** 27226.01-107-16  
**Project Name:** F-4500 Fiberglass Folding  
Doors (Impact)  
**Date:** 9/29/2023  
Page 2 of 15

**SCOPE:**

Molimo, LLC was contracted by Jeld-Wen Windows & Doors to evaluate alternate installation methods for their F-4500 Fiberglass Folding Doors (Impact). The evaluation is based on physical testing and product certifications.

Reference standards utilized in this project include:

*Florida Building Code.* International Code Council.

*ANSI/AWC National Design Specification (NDS) for Wood Construction.* American Wood Council.

*AISI S100 North American Specification for the Design of Cold-Formed Steel Structural Members.* American Iron and Steel Institute.

ICC-ES Report ESR-1976 ITW Buildex TEKS Self-Drilling Fasteners. ICC Evaluation Service.

NOA 21-0201.06 *Tapcon Concrete and Masonry Anchors with Advanced Threadform Technology.* Miami-Dade County Product Control Section.

The anchorage analysis presented herein does not address the water resistance, water penetration, or air infiltration performance of the installation method or the installed product. In addition, the analyses rely on the assumption that the building substrate is capable of withstanding the incurred loads.



**Project No.:** 27226.01-107-16  
**Project Name:** F-4500 Fiberglass Folding  
Doors (Impact)  
**Date:** 9/29/2023  
Page 3 of 15

### Certification of Independence

In accordance with Rule 61G20-3 Florida Administrative Code, Molimo, LLC hereby certifies the following:

- Molimo, LLC does not have, nor does it intend to acquire or will it acquire, a financial interest in any company manufacturing or distributing products tested or labeled by the agency.
- Molimo LLC is not owned, operated or controlled by any company manufacturing or distributing products it tests or labels.
- Michael D. Stremmel, P.E. does not have nor will acquire, a financial interest in any company manufacturing or distributing products for which the reports are being issued.
- Michael D. Stremmel, P.E. does not have, nor will acquire, a financial interest in any other entity involved in the approval process of the product.

## ANALYSES:

### Summary of Test Results

Table 1 summarizes the various F-4500 Fiberglass Folding Doors (Impact) products and their corresponding performance levels which have been established by testing or product certification.

**Table 1:** Summary of Test Results

| Series/Model   | Test Report Number   | Size (W x H)       | Performance                             |
|--|--|--------------------|---|
| F-4500 Fiberglass Folding<br>Impact Door<br>(Through Frame Installation) | Intertek Report No.<br>Q2461.01-301-47<br>(Rev. 0, 8/8/23) | 106-3/4" x 79-1/4" | +50 / -55 psf<br>Wind Zone 3<br>Impacts |

Testing documented in Table 1 was conducted by Intertek of Fresno, California (Florida Department of Business & Professional Regulation Test Lab No. TST2609, IAS Certificate of Accreditation TL-264) and certified by NAMI under certification number NI015728.01 (Expires 6/30/2027).

### As-Tested Installation Analysis

For air/water/structural testing, the test specimen was secured to a Douglas-Fir wood test buck with #8 wood screws (1-1/2" min embedment) at the head and jambs and a continuous bed of silicone at the sill. The as tested installation method is evaluated on Pages 5 through 7. These capacities will be used to prove acceptable anchors and substrates for the product.

### Alternate Anchorages

Calculations on Pages 8 through 15 determine the design capacity of alternate installation anchorages for the product.

### Anchorages Requirements

As-tested spacing must be maintained. It must be determined that the anchorages are not overloaded for the approved product size and design pressures. Calculations presented on Page 14 show the alternate anchorages are acceptable for the established product performance.

Anchorage requirements established by this report are accurately presented in Drawing D1000257.

### As-Tested Installation – Through Frame to Wood

#### Jamb Installation

Anchor: #8 Wood Screw

Details: 3/4" thick wood frame (G = 0.42)  
No shim space was utilized

Substrate: Douglas-Fir wood test buck (G = 0.46 min.)

#### Wood Screw Capacity (Shear)

$$Z' = \underline{111 \text{ lb}}$$

(See Page 6)

**Design Capacity of the Connection = 111 lb**

#### Head Installation

Anchor: #8 Wood Screw

Details: 0.063" aluminum frame (6063-T5)  
No shim space was utilized

Substrate: Douglas-Fir wood test buck (G = 0.46)

#### Wood Screw Capacity (Shear)

$$Z' = \underline{128 \text{ lb}}$$

(See Page 7)

#### Bearing Capacity (of #8 screw on aluminum frame)

$$P_b = 2 D t F_{tu} = 2(0.164")(0.063")(22,000 \text{ psi}) = \underline{454 \text{ lb}}$$

$$P_{\text{allow}} = 454 \text{ lb} / 3.0 = \underline{151 \text{ lb}}$$

**Design Capacity of the Connection = 128 lb**

## Lateral Design Strength of Wood Connections

### Data

|                    |   |                     |                                     |   |           |
|--------------------|---|---------------------|-------------------------------------|---|-----------|
| <b>Fastener</b>    |   |                     | <b>Project:</b> F-4500 Folding Door |   |           |
| Fastener           | = | #8 Wood Screw       | <b>Comments:</b> As-Tested (Jamb)   |   |           |
| Shank Dia          | = | 0.164 in.           | 1-1/2" min embedment                |   |           |
| Root Dia.          | = | 0.131 in.           |                                     |   |           |
| $F_{yb}$           | = | 90,000 psi          |                                     |   |           |
| Fastener length    | = | 2.250 in.           |                                     |   |           |
| <b>Main Member</b> |   |                     | <b>Side Member</b>                  |   |           |
| Material           | = | Douglas Fir (South) | Material                            | = | SPF       |
| G                  | = | 0.46                | G                                   | = | 0.42      |
| $\theta$           | = | 90                  | $\theta$                            | = | 90        |
| $F_e$              | = | 4,000 psi           | $F_{es}$                            | = | 3,350 psi |
| Thickness          | = | 1.500 in.           | Thickness                           | = | 0.719 in. |

### Calculations

#### Lateral Bearing Factors

|            |   |           |       |   |  |
|------------|---|-----------|-------|---|--|
| D          | = | 0.131 in. | $k_1$ | = | 0.6618   |
| $\ell_m$   | = | 1.203 in. | $k_2$ | = | 1.2340   |
| $K_\theta$ | = | 1.25      | $k_3$ | = | 1.29   |
| $K_D$      | = | 2.20      | $R_d$ | = | 2.20 (Mode I <sub>m</sub> , I <sub>s</sub> )         |
| $R_e$      | = | 1.194     | $R_d$ | = | 2.20 (Mode II)                                       |
| $R_t$      | = | 1.67      | $R_d$ | = | 2.20 (Mode III <sub>m</sub> , III <sub>s</sub> , IV) |

#### Lateral Design Values, Z

|                       |   |         |                   |
|-----------------------|---|---------|-------------------|
| Mode I <sub>m</sub>   | = | 287 lbf |                   |
| Mode I <sub>s</sub>   | = | 143 lbf |                   |
| Mode II               | = | 95 lbf  |                   |
| Mode III <sub>m</sub> | = | 104 lbf |                   |
| Mode III <sub>s</sub> | = | 69 lbf  | <== Minimum Value |
| Mode IV               | = | 82 lbf  |                   |

#### Adjustment Factors

|                        |   |                            |                                     |   |      |
|------------------------|---|----------------------------|-------------------------------------|---|------|
| $C_D$                  | = | 1.6                        | $C_\Delta$                          | = | 1.0  |
| Wet Service Factor     |   |                            | Is fastener installed in end grain? |   | No   |
| Fabrication/In-Service |   | Dry/Dry                    | $C_{eg}$                            | = | 1.00 |
| $C_M$                  | = | 1.0                        | Is fastener part of a diaphragm?    |   | No   |
| In service temperature |   | $T \leq 100^\circ\text{F}$ | $C_{di}$                            | = | 1.0  |
| $C_t$                  | = | 1.0                        | Is fastener toe-nailed?             |   | No   |
| $C_g$                  | = | 1.0                        | $C_{tn}$                            | = | 1.00 |

#### Adjusted Design Value, Z'

$$Z' = 111 \text{ lbf}$$

## Lateral Design Strength of Wood Connections

### Data

|                    |                       |                                     |
|--------------------|-----------------------|-------------------------------------|
| <b>Fastener</b>    |                       | <b>Project:</b> F-4500 Folding Door |
| Fastener           | = #8 Wood Screw       | <b>Comments:</b> As-Tested (Head)   |
| Shank Dia          | = 0.164 in.           | 1-1/2" min embedment                |
| Root Dia.          | = 0.131 in.           |                                     |
| $F_{yb}$           | = 90,000 psi          |                                     |
| Fastener length    | = 2.250 in.           |                                     |
| <b>Main Member</b> |                       | <b>Side Member</b>                  |
| Material           | = Douglas Fir (South) | Material                            |
| G                  | = 0.46                | G                                   |
| $\theta$           | = 90                  | $\theta$                            |
| $F_e$              | = 4,000 psi           | $F_{es}$                            |
| Thickness          | = 1.500 in.           | Thickness                           |
|                    |                       | 6063 T5 Aluminum                    |
|                    |                       | N/A                                 |
|                    |                       | 90                                  |
|                    |                       | 27,500 psi                          |
|                    |                       | 0.063 in.                           |

### Calculations

#### Lateral Bearing Factors

|            |             |       |          |   |
|------------|-------------|-------|----------|---|
| D          | = 0.131 in. | $k_1$ | = 1.3798 |   |
| $\ell_m$   | = 1.500 in. | $k_2$ | = 0.5616 |   |
| $K_\theta$ | = 1.25      | $k_3$ | = 11.45  |   |
| $K_D$      | = 2.20      | $R_d$ | = 2.20   | (Mode I <sub>m</sub> , I <sub>s</sub> )         |
| $R_e$      | = 0.145     | $R_d$ | = 2.20   | (Mode II)                                       |
| $R_t$      | = 23.81     | $R_d$ | = 2.20   | (Mode III <sub>m</sub> , III <sub>s</sub> , IV) |

#### Lateral Design Values, Z

|                       |           |                   |
|-----------------------|-----------|-------------------|
| Mode I <sub>m</sub>   | = 357 lbf |                   |
| Mode I <sub>s</sub>   | = 103 lbf |                   |
| Mode II               | = 142 lbf |                   |
| Mode III <sub>m</sub> | = 155 lbf |                   |
| Mode III <sub>s</sub> | = 80 lbf  | <== Minimum Value |
| Mode IV               | = 113 lbf |                   |

#### Adjustment Factors

|                        |                            |                                     |        |
|------------------------|----------------------------|-------------------------------------|--------|
| $C_D$                  | = 1.6                      | $C_\Delta$                          | = 1.0  |
| Wet Service Factor     |                            | Is fastener installed in end grain? | No     |
| Fabrication/In-Service | Dry/Dry                    | $C_{eg}$                            | = 1.00 |
| $C_M$                  | = 1.0                      | Is fastener part of a diaphragm?    | No     |
| In service temperature | $T \leq 100^\circ\text{F}$ | $C_{di}$                            | = 1.0  |
| $C_t$                  | = 1.0                      | Is fastener toe-nailed?             | No     |
| $C_g$                  | = 1.0                      | $C_{tn}$                            | = 1.00 |

#### Adjusted Design Value, Z'

|    |           |
|----|-----------|
| Z' | = 128 lbf |
|----|-----------|

### Alternate Installation – Strap Anchor to Wood

Anchor: (2) #8 x 1-1/2" Flat head screw securing the strap to the substrate  
1/4" max shim space

Details: 20 gauge (0.036" thick) 33 KSI steel strap anchor w/ two #8 screws securing the  
strap to the frame  
3/4" thick wood frame -- or -- 0.063" 6063-T5 Aluminum

Substrate: Spruce-Pine-Fir 2x Wood Substrate (G = 0.42 min.)

#### Wood Screw Capacity (Shear)

$$Z' = \underline{122 \text{ lb}}$$

(See Following Page)

#### Bending of #8 x 1-1/2" flat head screw

$$L = 1/4" \text{ (maximum shim space)}$$

$$S = \pi d^3 / 32 = \pi (0.131")^3 / 32 = 0.000221 \text{ in}^3$$

$$F_b = (1.3)(0.6 F_y) = (1.3)(0.6)(90,000 \text{ psi}) = 70,200 \text{ psi} \quad (1.3 \text{ for weak axis bending})$$

$$F_b = M / S = (V) (L/2) / S \quad (L/2 \text{ for guided bending})$$

$$V = 2 S F_b / L = (2)(0.000221 \text{ in}^3)(70,200 \text{ psi}) / 1/4"$$

$$V = \underline{124 \text{ lb}}$$

#### Bearing Capacity (of #8 screw on aluminum frame)

$$P_b = 2 D t F_{tu} = 2(0.164")(0.063")(22,000 \text{ psi}) = \underline{454 \text{ lb}}$$

$$P_{\text{allow}} = 454 \text{ lb} / 3.0 = \underline{151 \text{ lb}}$$

#### Bearing Capacity (of strap anchor)

$$P_b = 2.7 D t F_{tu} = 2.7(0.164")(0.036")(45,000 \text{ psi}) = 717 \text{ lb}$$

$$P_{\text{allow}} = 717 \text{ lb} / 3.0 = \underline{239 \text{ lb}}$$

**Design Capacity of the Connection = 122 lb per screw (244 lb total)**



## Lateral Design Strength of Wood Connections

### Data

| <b>Fastener</b> |                 |
|-----------------|-----------------|
| Fastener        | = #8 Wood Screw |
| Shank Dia       | = 0.164 in.     |
| Root Dia.       | = 0.131 in.     |
| $F_{yb}$        | = 90,000 psi    |
| Fastener length | = 1.500 in.     |

**Project:** F-4500 Folding Door  
**Comments:** Anchor Strap Detail  
 1-1/2" min embedment

| <b>Main Member</b> |             |
|--------------------|-------------|
| Material           | = SPF       |
| G                  | = 0.42      |
| $\theta$           | = 90        |
| $F_e$              | = 3,350 psi |
| Thickness          | = 1.500 in. |

| <b>Side Member</b> |                              |
|--------------------|------------------------------|
| Material           | = ASTM A 653, Grade 33 Steel |
| G                  | = N/A                        |
| $\theta$           | = 90                         |
| $F_{es}$           | = 61,850 psi                 |
| Thickness          | = 0.033 in.                  |

### Calculations

#### Lateral Bearing Factors

|            |             |       |  |
|------------|-------------|-------|--|
| D          | = 0.131 in. | $k_1$ | = 0.7630   |
| $\ell_m$   | = 1.139 in. | $k_2$ | = 0.5398   |
| $K_\theta$ | = 1.25      | $k_3$ | = 23.87  |
| $K_D$      | = 2.20      | $R_d$ | = 2.20 (Mode I <sub>m</sub> , I <sub>s</sub> )         |
| $R_e$      | = 0.054     | $R_d$ | = 2.20 (Mode II)                                       |
| $R_t$      | = 34.52     | $R_d$ | = 2.20 (Mode III <sub>m</sub> , III <sub>s</sub> , IV) |

#### Lateral Design Values, Z

|                       |           |
|-----------------------|-----------|
| Mode I <sub>m</sub>   | = 227 lbf |
| Mode I <sub>s</sub>   | = 122 lbf |
| Mode II               | = 93 lbf  |
| Mode III <sub>m</sub> | = 111 lbf |
| Mode III <sub>s</sub> | = 77 lbf  |
| Mode IV               | = 108 lbf |

<== Minimum Value

#### Adjustment Factors

|                        |           |                                     |        |
|------------------------|-----------|-------------------------------------|--------|
| $C_D$                  | = 1.6     | $C_\Delta$                          | = 1.0  |
| Wet Service Factor     |           | Is fastener installed in end grain? | No     |
| Fabrication/In-Service | Dry/Dry   | $C_{eg}$                            | = 1.00 |
| $C_M$                  | = 1.0     | Is fastener part of a diaphragm?    | No     |
| In service temperature | T ≤ 100°F | $C_{di}$                            | = 1.0  |
| $C_t$                  | = 1.0     | Is fastener toe-nailed?             | No     |
| $C_g$                  | = 1.0     | $C_{tn}$                            | = 1.00 |

#### Adjusted Design Value, Z'

$Z'$  = 122 lbf

**Alternate Installation – Through-Frame to Concrete**

Anchor: 3/16" Tapcon Anchor  
- 1-1/4" min embedment  
- 2-1/2" min edge distance  
- 3" min anchor spacing  
- 1/4" max shim space

Details: Through the Wood or Aluminum Frame  
- 3/4 " thick wood frame  
- 0.063" thick aluminum frame (6063-T5)

Substrate: 3,000 psi Concrete

**Anchor Capacity** (Shear of 3/16" Tapcon)

$$P_{ss} / \Omega = \underline{181 \text{ lb}} \quad (\text{NOA-No. 21-0201.06})$$

**Bearing Capacity** (of Wood frame)

$$P_b = F_e D t / K_D = (3,350 \text{ psi})(0.170")(0.719") / (10(0.170) + 0.5) = \underline{194 \text{ lb}}$$

**Bearing Capacity** (of Aluminum frame)

$$P_b = 2 D t F_{tu} = 2(0.170")(0.063")(22,000 \text{ psi}) = 471 \text{ lb}$$

$$P_{\text{allow}} = 471 \text{ lb} / 3.0 = \underline{157 \text{ lb}}$$

**Bending Capacity** (of 3/16" Tapcon)

$$L = 1/4" \text{ (maximum shim space)}$$

$$S = \pi d^3 / 32 = \pi (0.170")^3 / 32 = 0.000482 \text{ in}^3$$

$$F_b = (1.3)(0.6 F_y) = (1.3)(0.6)(137,000 \text{ psi}) = 106,860 \text{ psi} \quad (1.3 \text{ for weak axis bending})$$

$$F_b = M / S = (V) (L/2) / S \quad (L/2 \text{ for guided bending})$$

$$V = 2 S F_b / L = (2)(0.000482 \text{ in}^3)(106,860 \text{ psi}) / 1/4"$$

$$V = \underline{412 \text{ lb}}$$

**Design Capacity of the Connection = 157 lb**

**Qualifies 1/4" Tapcon if longer length anchor is required to achieve minimum embedment**

**Alternate Installation – Through-Frame to CMU Block**

Anchor: 3/16" Tapcon Anchor  
- 1-1/4" min embedment  
- 2-1/2" min edge distance  
- 3" min anchor spacing  
- 1/4" max shim space

Details: Through the Wood or Aluminum Frame  
- 3/4 " thick wood frame  
- 0.063" thick aluminum frame (6063-T5)

Substrate: CMU Block

Anchor Capacity (Shear of 3/16" Tapcon)

$$P_{ss} / \Omega = \underline{135 \text{ lb}} \quad (\text{NOA-No. 21-0201.06})$$

Bearing Capacity (of Wood frame)

$$P_b = F_e D t / K_D = (3,350 \text{ psi})(0.170")(0.719") / (10(0.170) + 0.5) = \underline{194 \text{ lb}}$$

Bearing Capacity (of Aluminum frame)

$$P_b = 2 D t F_{tu} = 2(0.170")(0.063")(22,000 \text{ psi}) = 471 \text{ lb}$$

$$P_{\text{allow}} = 471 \text{ lb} / 3.0 = \underline{157 \text{ lb}}$$

Bending Capacity (of 3/16" Tapcon)

$$L = 1/4" \text{ (maximum shim space)}$$

$$S = \pi d^3 / 32 = \pi (0.170")^3 / 32 = 0.000482 \text{ in}^3$$

$$F_b = (1.3)(0.6 F_y) = (1.3)(0.6)(137,000 \text{ psi}) = 106,860 \text{ psi} \quad (1.3 \text{ for weak axis bending})$$

$$F_b = M / S = (V) (L/2) / S \quad (L/2 \text{ for guided bending})$$

$$V = 2 S F_b / L = (2)(0.000482 \text{ in}^3)(106,860 \text{ psi}) / 1/4"$$

$$V = \underline{412 \text{ lb}}$$

**Design Capacity of the Connection = 135 lb**

**Qualifies 1/4" Tapcon if longer length anchor is required to achieve minimum embedment**

### Alternate Installation – Strap Anchor to Concrete

**Anchor:** 3/16" Tapcon Anchor  
 - 1-1/4" min embedment  
 - 2-1/2" min edge distance  
 - 3" min anchor spacing  
 - 1/4" max shim space

**Details:** 20 gauge (0.036" thick) 33 KSI steel strap anchor w/ two #8 screws securing the strap to the frame  
 3/4" thick wood frame -- or -- 0.063" 6063-T5 Aluminum

**Substrate:** 3,000 psi Concrete

#### Anchor Capacity (Shear of 3/16" Tapcon)

$$P_{ss} / \Omega = \underline{181 \text{ lb}} \quad (\text{NOA-No. 21-0201.06})$$

#### Bearing Capacity (of 3/16" Tapcon on strap anchor)

$$P_b = 2.7 D t F_{tu} / \Omega = 2.7(0.170")(0.036")(45,000 \text{ psi}) / 3.0 = \underline{247 \text{ lb}}$$

#### Bearing Capacity (of #8 screw on strap anchor)

$$P_b = 2.7 D t F_{tu} / \Omega = 2.7(0.164")(0.036")(45,000 \text{ psi}) / 3.0 = \underline{239 \text{ lb}}$$

#### Bearing Capacity (of #8 screw on wood frame)

$$P_b = F_e D t / K_D = (3,350 \text{ psi})(0.164")(0.719") / (10(0.164) + 0.5) = \underline{184 \text{ lb}}$$

#### Bearing Capacity (of #8 screw on Aluminum frame)

$$P_b = 2 D t F_{tu} / \Omega = 2(0.170")(0.063")(22,000 \text{ psi}) / 3.0 = \underline{157 \text{ lb}}$$

#### Bending Capacity (of 3/16" Tapcon)

$$L = 1/4" \text{ (maximum shim space)}$$

$$S = \pi d^3 / 32 = \pi (0.170")^3 / 32 = 0.000482 \text{ in}^3$$

$$F_b = (1.3)(0.6 F_y) = (1.3)(0.6)(137,000 \text{ psi}) = 106,860 \text{ psi} \quad (1.3 \text{ for weak axis bending})$$

$$F_b = M / S = (V) (L/2) / S \quad (L/2 \text{ for guided bending})$$

$$V = 2 S F_b / L = (2)(0.000482 \text{ in}^3)(106,860 \text{ psi}) / 1/4"$$

$$V = \underline{412 \text{ lb}}$$

**Design Capacity of the Connection = 157 lb (one concrete anchor per strap)**

**Qualifies 1/4" Tapcon if longer length anchor is required to achieve minimum embedment**

**Alternate Installation – Strap Anchor to CMU Block**

Anchor: 3/16" Tapcon Anchor  
 - 1-1/4" min embedment  
 - 2-1/2" min edge distance  
 - 3" min anchor spacing  
 - 1/4" max shim space

Details: 20 gauge (0.036" thick) 33 KSI steel strap anchor w/ two #8 screws securing the strap to the frame  
 3/4" thick wood frame -- or -- 0.063" 6063-T5 Aluminum

Substrate: CMU Block

Anchor Capacity (Shear of 3/16" Tapcon)

$$P_{ss} / \Omega = \underline{135 \text{ lb}} \quad (\text{NOA-No. 21-0201.06})$$

Bearing Capacity (of 3/16" Tapcon on strap anchor)

$$P_b = 2.7 D t F_{tu} / \Omega = 2.7(0.170")(0.036")(45,000 \text{ psi}) / 3.0 = \underline{247 \text{ lb}}$$

Bearing Capacity (of #8 screw on strap anchor)

$$P_b = 2.7 D t F_{tu} / \Omega = 2.7(0.164")(0.036")(45,000 \text{ psi}) / 3.0 = \underline{239 \text{ lb}}$$

Bearing Capacity (of #8 screw on wood frame)

$$P_b = F_e D t / K_D = (3,350 \text{ psi})(0.164")(0.719") / (10(0.164) + 0.5) = \underline{184 \text{ lb}}$$

Bearing Capacity (of Aluminum frame)

$$P_b = 2 D t F_{tu} / \Omega = 2(0.170")(0.063")(22,000 \text{ psi}) / 3.0 = \underline{157 \text{ lb}}$$

Bending Capacity (of 3/16" Tapcon)

$$L = 1/4" \text{ (maximum shim space)}$$

$$S = \pi d^3 / 32 = \pi (0.170")^3 / 32 = 0.000482 \text{ in}^3$$

$$F_b = (1.3)(0.6 F_y) = (1.3)(0.6)(137,000 \text{ psi}) = 106,860 \text{ psi} \quad (1.3 \text{ for weak axis bending})$$

$$F_b = M / S = (V) (L/2) / S \quad (L/2 \text{ for guided bending})$$

$$V = 2 S F_b / L = (2)(0.000482 \text{ in}^3)(106,860 \text{ psi}) / 1/4"$$

$$V = \underline{412 \text{ lb}}$$

**Design Capacity of the Connection = 135 lb (one concrete anchor per strap)**

**Qualifies 1/4" Tapcon if longer length anchor is required to achieve minimum embedment**

**Alternate Installation – Strap Anchor to Wood (Cap Installation)**

**Anchor:** Two #8 x 1-1/2" Flat head screw securing the strap to the substrate

**Details:** 20 gauge (0.036" thick) 33 KSI steel strap anchor w/ two #8 screws securing the strap to the frame

0.719" thick wood frame

3/4" thick wood frame -- or -- 0.063" 6063-T5 Aluminum

**Substrate:** Spruce-Pine-Fir 2x Wood Substrate (G = 0.42 min.)

**Wood Screw Capacity (Withdrawal)**

$$W' = 1.6(82 \text{ lb/in})(1.5 \text{ in}) = \underline{197 \text{ lb}}$$

**Pull-over Capacity (of #8 screw on strap)**

$$P_{\text{nov}} = 1.5 t d F_{\text{tu}} = 1.5 (0.036")(0.332")(45,000 \text{ psi}) = 806 \text{ lb}$$

$$P_{\text{allow}} = 806 \text{ lb} / 3.0 = \underline{268 \text{ lb}}$$

**Bearing Capacity (of #8 screw on wood frame)**

$$P_b = F_e D t / K_D = (3,350 \text{ psi})(0.164")(0.719") / (10(0.164) + 0.5) = \underline{184 \text{ lb}}$$

**Bearing Capacity (of #8 screw Aluminum frame)**

$$P_b = 2 D t F_{\text{tu}} / \Omega = 2(0.170")(0.063")(22,000 \text{ psi}) / 3.0 = \underline{157 \text{ lb}}$$

**Bearing Capacity (of #8 screw on strap anchor)**

$$P_b = 2.7 D t F_{\text{tu}} = 2.7(0.164")(0.036")(45,000 \text{ psi}) = 717 \text{ lb}$$

$$P_{\text{allow}} = 717 \text{ lb} / 3.0 = \underline{239 \text{ lb}}$$

**Design Capacity of the Connection = 157 lb (one screw)**

**Design Capacity of the Connection = 314 lb (two screws)**

### Anchorage Requirements

Series/Model: F-4500 Fiberglass Folding Impact Doors  
Test Unit Size: 106-3/4" x 79-1/4"  
Design Pressure: +50.0 / -55.0 psf

### Through-Frame Installation Method

Through frame installation method is validated by the test

Through Frame Anchor Capacity = 111 lb / anchor (Head)  
= 128 lb / anchor (Jamb)

### Alternate Installation Methods

Strap Anchor to Wood = 122 lb / anchor – 244 lb total (Head or Jamb)

Through-Frame to Concrete = 157 lb (Head)  
= 181 lb (Jamb)

Through-Frame to CMU Block = 135 lb (Head or Jamb)

Strap Anchor to Concrete = 157 lb (Head)  
= 181 lb (Jamb)

Strap Anchor to CMU Block = 135 lb / anchor (Head or Jamb)

Strap Anchor to Wood (Cap Installation) = 157 lb / anchor (Head)  
= 184 lb / anchor (Jamb)

Minimum Alternate Installation Capacity = 135 lb

135 lb > 111 lb

**Head Alternate Anchorages OK at tested spacing**

135 lb > 128 lb

**Jamb Alternate Anchorages OK at tested spacing**



**Project No.:** 27226.01-107-16  
**Project Name:** F-4500 Fiberglass Folding  
Doors (Impact)  
**Date:** 9/29/2023

### Revision Log

| <b>Rev. #</b> | <b>Date</b> | <b>Page(s)</b> | <b>Revision(s)</b>    |
|---------------|-------------|----------------|-----------------------|
| 0             | 9/29/2023   | All            | Original Report Issue |